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FEDERAL COMMENT

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CONVENTION AGENDA

As Easter once more approaches, we realise that another Federal Convention is about to take place—this year in Queensland—and as far as records show, the first time ever in that State. For some time prior to the Convention, Divisions have been literally scratching their heads wondering what they shall raise in the way of Agenda items.

It has been evident for many years that a number of items in the category of "hardy annuals" will again appear and that yet others will have been hastily thought of at the last minute and included in an effort to save "Divisional face". Whilst the latter situation should be avoided to save valuable time at Conventions, these items nonetheless receive the same attention and consideration as well-thought-out motions dealing with the more important and urgent matters of policy.

The Oxford Dictionary defines a Convention as a formal assembly for deliberation or legislation on important matters and further as an assembly of delegates or representatives at conference. While the stress is on the discussion of "important matters," there are other benefits to be derived from a Convention which are not revealed in definitions. These are the meeting of the delegates in person and being able to discuss both formally and informally mutual problems. It is also being able to inform the other delegates of the background to certain motions which may appear both specious and unimportant on paper. Despite these additional benefits from Conventions, a number of relatively unimportant matters still appear year after year which could be just as easily conveyed in writing during the year.

The foundations of our Institute are now quite old and we should now be grown-up enough to base future Conventions on policy and important administrative matters which are not easily sorted out by correspondence. Matters dealing with the Constitution, attracting new members, new types of licence, regulatory matters of Amateur operation are all subjects on which more time could be spent with profit at the Conference table without the Chairman having to hurry discussion along to more mundane and trivial matters.

The matter rests entirely in the hands of the Divisions as to what matters they commit to Convention agenda or submit by correspondence. The attitude should not be—we will look foolish if we don't submit about ten items; it should be—can we get an answer to this problem by postal motion or is it contentious enough for discussion at a Convention. The guiding thought for the future should be—one good motion on the agenda is worth ten trivial motions.

—W. T. S. MITCHELL, FEDERAL COMMUNICATIONS MANAGER.

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MODIFYING THE PALEC VALVE AND CIRCUIT TESTER

G. WALL*

IF you have a "Palec" VCT or VCT-V you most likely have lamented the fact that it has not been able to keep pace with the output of modern valve types.

It is probable that you have also contemplated or obtained adaptor panels or adaptor panels, only to find that they, too, have been outmoded by later types of valves.

This trend can keep on going, and probably will "ad infinitum" or "ad nauseum," depending on your point of view.

The first problem in modifying the unit was "how many switches?" This presented a problem, because how many valve connections are the future valves going to have? Our "crystal ball" video circuits broke down, but as advertisements for 10-pin types have been seen, it was decided that this should be a start.

A 12-pin socket and plug were obtained and installed on the front panel to connect the adaptor panels into the tester, this then prompted the installation of 12 switches, and although a

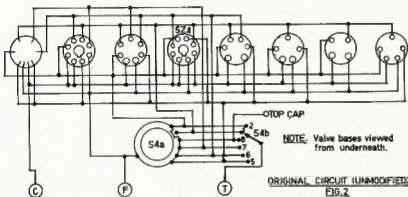
centre of the meter, approximately 3½ inches from the top of the panel. Cut a suitable piece of metal to fit the space from this position to the top of the panel.

Mount the switches on this sub-panel, either side of the meter opening, and after cutting the original panel to accommodate the switches, fix the sub-panel in place.

With the switches mounted in position, thread a wire (18-16 s.w.g. tinned copper) through the switch lugs as shown in Fig. 3 and reconnect to the original tester circuits removed from the valve sockets and element short switch, as designated (F) Filament, (C) Common, and (T) Test.

Bridge lugs 1 and 7 (Fig. 3) on each switch, as viewed from the top of panel and connect this bridge wire to the appropriate valve pin and 12-pin socket pins, left on the top panel, for extension to the external adaptor panels.

The circuit of Fig. 4 shows the actual switch connections, for two of the four positions of each switch, from which it will be seen how each valve element can be selected, to be (A) left connected to common filament; (B) left in an open position; (C) selected for filament voltage, or (D) selected for test, for either "emission" or "element short", depending on the position of the function switch selector at the bottom l.h.s. of the unit.



ORIGINAL CIRCUIT (UNMODIFIED)
FIG. 2

The main trouble with the valve tester (Palec) is that where valves have electrodes connected to more than one base pin the tester will show an "element short" and in most cases cannot be tested.

While this instrument is not the ultimate in valve testing, there is no doubt that it is still a useful piece of equipment. It has retained its usefulness and its value even second or third hand from the original purchaser.

As new, these units were approximately £21-£22, and 20 to 25 years later still cost about £10 to £15 secondhand, depending on condition, furthermore the demand exceeds the supply.

With this in mind, prompted by a modern type with switching to isolate each valve element, enquiries were made to find some of these switches to bring the "Palec" up to date, to cope with as many valve types, past, present and future.

Finally, it was found that "Astronic Imports" (Melb.) had a few, but obligingly obtained a complete set of "Tech" TC-2, 2-pole 4-position, slide-type switches for the job, also a few more for stock, and mentioned that more could be obtained freely if required.

Your adaptor panels will still be required, because when the switches are installed in the front panel, there is no room for more than a couple of valve sockets, but valves with electrodes connected to more than one pin can be tested with the modified unit.

tight squeeze on the "Palec" front panel, six switches can be put either side of the meter at the top of the panel.

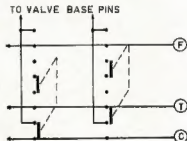
How each individual modifies his unit may vary a little, but as space is limited it is suggested that the following be given some thought.

Remove all valve sockets as a start, together with the "Selector Switch" (S4a-S4b) as this will no longer be required. (See Fig. 2.)

Move the "Ohms Adj." pot. into the "Element Selector Switch" position, and install the neon test lamp into the "Ohms Adj." hole.

The top cap connection can be moved to any convenient position or beside the neon globe and will clear the top of the panel for the switches.

In most "Palec" testers there is a plated or painted strip just above the



SCHEMATIC SWITCHING CIRCUIT
FIG. 4

To enable you to follow the switching, and for trouble shooting, the complete circuit has been included (Fig. 1) (we think for the first time) together with component values.

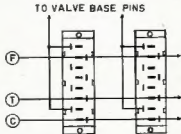
After having completed the wiring modification and re-checking, tests may be made.

While most owners of these units will be conversant with the testing drill of the original wiring, a few suggestions in operation for the sake of completeness are added.

To test valves: Set all switches in the common position.

Set selector switch to "Line switch," adjust "Line Adj." to full scale meter deflection.

Ascertain to which pins the valve filaments are connected, set filament



REAR VIEW OF
ELEMENT SELECTOR SWITCH
FIG. 3

(Continued on Page 14)

* 34 Railway Crescent, Moorabbin, Vic.

ELEMENT SELECTOR SWITCH CONNECTIONS TO CORRESPONDING PIN OF ALL VALVE SOCKETS

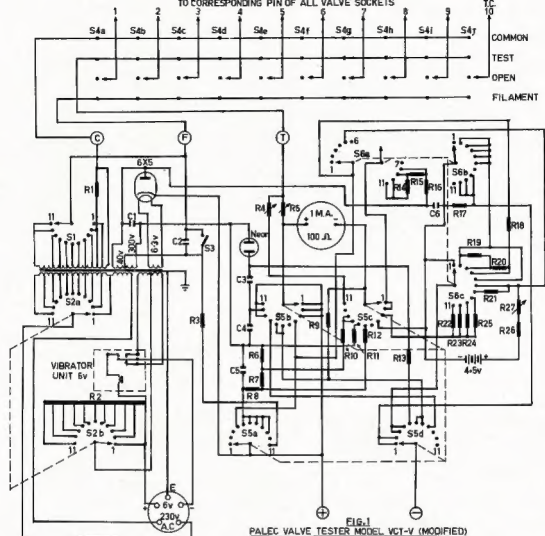


FIG. 1
PALEC VALVE TESTER MODEL VCT-V (MODIFIED)

CONDENSERS

C1—0.01 μ F, 2000v.
C2—0.01 μ F, 350v.
C3—0.01 μ F, 350v.
C4—0.009 μ F, 350v.
C5—0.5 μ F, 350v.
C6—2.0 μ F, 350v.

RESISTORS

R1—1.0 ohms
R2—0.82 ohms total
R3—25K
R4—250 ohms w.w.
R5—50 ohms range
R6—6K
R7—25K
R8—4K
R9—20 ohms
R10—225K
R11—50K
R12—25K
R13—25K
R14—210K
R15—125K
R16—6.6K
R17—253K
R18—0.444 ohms
R19—10 ohms
R20—0.897 ohms
R21—2.8K
R22—1 meg.
R23—250K

R24—100K

R25—9.55K
R26—300 ohms
R27—1K var.

SWITCHES

S1—Filament Volts.
1 1.4 volts
2 2.0 "
3 2.5 "
4 3.2 "
5 4.0 "
6 5.0 "
7 6.3 "
8 7.5 "
9 12.5 "
10 25.0 "
11 25.0 "
S2—Line Adjust.
1 150 volts
2 200 "
3 250 "
4 320 "
5 225 "
6 230 "
7 235 "
8 240 "
9 245 "
10 250 "
11 250 "
S3—Press for Merit

S4—Selector.

Section S4b connects one valve element to meter or neon whilst S4a connects the remainder to filament volts a.c.
Note: S4a and b is replaced in modified circuit with switches S4a b c d e f g h i j.

S5—e b c d.

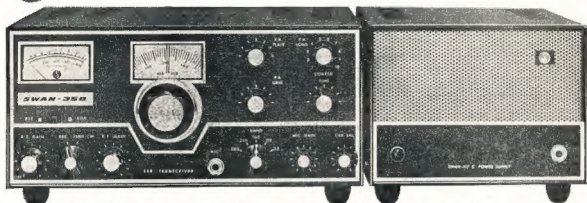
1 output volts
2 a.c. volts
3 d.c. volts
4 mA—ohms
5 Paper condensers
6 Electrolytic—50v.
7 Electrolytic—800v.
8 Megohms
9 Line Check
10 Element Shorts
11 Merit Test

S6—a b c.

(Section a 2—5 x 1 successive).
(Section b, c 2—11 x 1).
1 1 mA.
2 10 mA.
3 100 mA.
4 250 mA.
5 Low ohms
6 Ohms x 10
7 10 volts
8 100 volts
9 250 volts
10 500 volts
11 1000 volts



"SWAN" NEWS



Congratulations to the organisers of the Gosford Field Day, a really wonderful day greatly enjoyed by everybody including the writer. This show is one of the best, if not the best we have attended, especially good wishes to the XYLY's for their wonderful catering.

Of course "SWAN" was there, in cars, and on our stand were several SW350 transceivers and associated equipment. Some sets were partially dismantled so that the very excellent workmanship and high quality components of this equipment could be admired. Good DX was worked all day from 8.30 in the morning until 4.30 in the afternoon, the most distant stations worked being: Spain EAB, Alaska and Laos, and of course many W and Pacific Island stations. Most people were astounded at the results obtained on our lowly Dipole antenna, approximately 8 ft. to 10 ft. high, but this is common practice with the Swan SW350 and SW400 transceivers as anyone who sees us at radio shows will admit.

We have just been advised that the U.S. Navy has placed orders for Swan equipment as back up for Collins, so with the tremendous popularity of the SW350 Swan are indeed very busy. Do you know that one person in 10 at Swan is engaged in quality control? This accounts for the extremely high quality of this equipment.

New Products: All band mobile whips, both automatic and manual adjustment type, composite power supplies, both 240v. a.c. and 12v. d.c. New SW410 5 band full coverage V.F.O. Keep your eyes peeled on this page for announcement on V.H.F. Transceivers. 12V.

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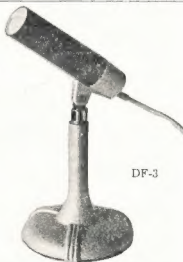
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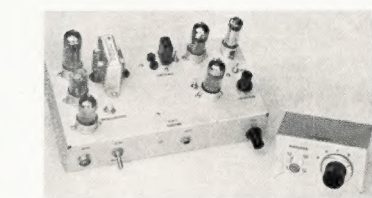
Agents: D. K. Northover & Co.; Neil Muller Ltd.; Homecrafts (Tas.) P/L; Jacoby, Mitchell & Co. P/L; T. H. Martin P/L.

AN A.M.-C.W. EXCITER FOR 144 Mc.*

A CLEAN SIGNAL FOR THE AB1 LINEAR

DOUG DeMAW, WICER

The exciter described in this article will provide a chirp-free, shaped c.w. note and will produce a well-modulated a.m. signal. Used either as a low-power transmitter, or as a driver for an a.m. linear amplifier, this unit can satisfy a host of needs in the v.h.f. station. R.f. isolation protects the speech and modulator stages from the feedback ill-effects that are common to many v.h.f. phone rigs.



A top-chassis view of the low-power exciter. Shown at the right—a 5-watt step attenuator for reducing the output of the exciter when used with a linear amplifier.

A GREAT deal of information has been published with regard to proper operation of linear amplifiers, but some Radio Amateurs are not aware of the importance of the signal quality required from the exciter unit. Unfortunately, the defects present in the output signal of the exciter are magnified by the linear amplifier. Because of this, a number of somewhat horrendous signals are heard on the various Amateur Radio bands. For a.m. linear operation, the r.f. output from the exciter must be free from hum, spurious energy and improper modulation characteristics. The c.w. signal, which is used to excite the linear amplifier, must be similarly clean, and without key clicks and thumps.

This article describes a low-power a.m./c.w. exciter, tailored to use with Class AB1 linear amplifiers, and capable of producing a clean excitation source for this mode of operation. A description of an attenuator box is included in the text. It will permit swamping out of excessive driving power to the amplifier used, and is suitable for a.m. or c.w. operation. It will work well with the equipment described in this article, but can also be used with other exciter/linear-amplifier combinations.

THE CIRCUIT

Two 6CX8 tubes are employed in the r.f. section of the exciter (Fig. 2). Sufficient power output is developed to fully excite a 4CX250 tube, operating in the AB1 mode. A regulated screen voltage is supplied to the oscillator stage (V1A) to prevent chirp, caused by the changes in power-supply voltage, during c.w. operation. This same feature contributes to better stability of the a.m. signal. The crystal v.f.o. switch, S1, converts V1A from an oscillator to an amplifier when the switch is placed in the v.f.o. position. An external v.f.o. can then be attached at J1, supplying an 8 or 24-Mc. signal to the exciter. With S1 in the crystal position (open), standard 8-Mc. crystals can be used for frequency con-

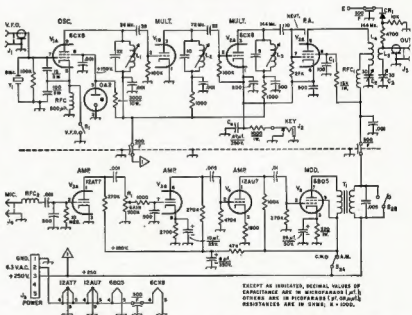


Fig. 2—Schematic diagram of the 3-meter assembly. Resistors are 1/4-watt composition type unless otherwise noted. Capacitors are disc ceramic except those bearing polarity markings, which are electrolytic. F indicates feedthrough type. SM is silver mica.

- CI—100-pf. disc ceramic with pigtail cut to 1/4-inch length.
- C2, C3—30 p.f. variable (Hammarlund MAC-20).
- C4—47-μf. mylar or moulded paper capacitor.
- CR1—1N34A.
- E—On terminal of feedthrough capacitor.
- J1—BNC chassis receptacle (UG-200/U).
- J2—Closed-circuit key jack.
- J3—Co-axial chassis connector (SO-239).
- J4—Microphone connector.
- J5—5-pin male chassis connector (Amphenol 86-CP5).
- L1—11 turns No. 24 enam. close wound on 3/4-inch diam. iron-slug form.
- L3—5 turns No. 24 enam. close wound on 1/4-inch diam. iron-slug form.

- L5—2 turns No. 20 bus wire, spaced to occupy 1/4-inch area on 1/4-inch diam. iron-slug form.
- L4—6 turns No. 20 bus, 1/4-inch diam. × 1 inch long, centre tapped.
- L5—2 turns No. 22 insulated hook-up wire, 1/4-inch diam. inserted into centre of L4.
- R1—0.5 megohm control, audio taper.
- RF1, RF2—1.8-μh. r.f. choke (Ohmite Z-144).
- S1—S.p.s.t. slide switch.
- S2—D.p.s.t. toggle switch.
- T1—5-watt modulation transformer (8tancon A-312 using one half of centre-tapped winding as primary).
- Y1—8-Mc. fundamental crystal.

* Reprinted from "QST," Sept. 1965.

trol. The tuned circuits, L1, L2 and L3, have sufficiently broad response to permit output frequency excursions of 1 Mc. without need for retuning the stages. A gimmick capacitor is used to neutralise the p.a. stage (V20) and is necessary if stable operation is to be secured. The screen-grid capacitor, C1, is series-resonant at 144 Mc. and aids in stabilisation of the output stage. For c.w. operation, the cathodes of V2A and V2B are connected in parallel and keyed at J2. A shaping network, consisting of a 0.47 μ F. capacitor and a 1000-ohm resistor, is connected between the keyed cathodes and the key jack. This network eliminates make-and-break clicks, resulting in a well-shaped keying characteristic. An r.f.-sampling test point (E) is available for tuneup of the exciter.

Special attention was given to the audio section of the exciter in an effort to reduce distortion to a minimum, while making certain that 100 per cent. modulation was possible. The modulator is capable of producing far more audio than is necessary, which permits the 6BQ5 tube to operate below the point where distortion becomes a significant consideration. R.f. filtering is used at J4, and at the grid of V3B, to prevent the squealing and howling common to many v.h.f. transmitters. Additional r.f. isolation is offered by the shield partition which divides the two halves of the chassis. The inter-circuit wiring which passes through this shield, is routed through FT (feed-through) capacitors to aid further in decoupling. Three stages of speech amplification are used, to avoid having marginal speech gain—a shortcoming of many v.h.f. transmitters. The values chosen for the coupling capacitors, grid resistors and plate resistors in the modulator will provide optimum response in the 400 to 3000-cycle range. This system helps to eliminate the hum component in the signal, while passing the most effective portion of

the voice range. Switch S2 disables the modulator during c.w. operation and shorts out the secondary winding of T1.

The power supply requirements for the exciter are 250 volts at 150 Ma. and 6.3 volts at 3 amperes. A measured r.f. power output of 2.1 watts was secured using a Thurline watt-meter terminated by a 50-ohm non-inductive dummy load.

CONSTRUCTION

The 2-meter exciter is built on a 9 $\frac{1}{2}$ x 5 x 2-inch aluminum chassis. The circuit wiring in the r.f. section of the chassis should be carried out in the manner shown in Fig. 3. All leads carrying r.f. should be kept short and

direct as possible, to maintain the possibility of stray inductance. Similar treatment should be given to the leads on the various bypass capacitors and resistors used in the r.f. circuitry.

Two crystal sockets are mounted on the chassis to facilitate using both the popular FT-243 units and the less-common pin size of another war-surplus type crystal. Since the latter was added as a convenience for the author, it is not necessary for the constructor to include the extra socket.

The v.f.o. input jack, J1, and the crystal/v.f.o. switch are located on the rear apron of the chassis near V1. Ceramic tube sockets are used at V1 and V2, reducing r.f. losses in that part of the circuit. The key jack and its related shaping network are near the front edge of the chassis. The plate-tank inductor and capacitors C2 and C3 are to the left of this area (Fig. 3). The r.f. output jack, J3, is located on the rear of the chassis and is connected to L3 through a short length of 50-ohm subminiature co-axial cable.

Turning next to the audio portion of the assembly, the microphone conductor and phone/c.w. switch are on the front wall of the chassis. The modulation level control is mounted on the top surface of the chassis and is adjacent to V3 and S2. The power-supply connector, J5, is located on the rear wall of the chassis, near the 6BQ5 modulator tube. Test point E is between C3 and OA2 voltage-regulator tube. An aluminum plate, with four rubber feet attached, is used to enclose the bottom of the chassis after the final testing is completed.

TUNE-UP AND OPERATION

Prior to applying the B-plus and filament voltages to the completed exciter, place the tubes in their sockets and adjust coils L1, L2 and L3 to resonance with a grid-dip meter. The correct frequency for each of these inductors is shown in Fig. 2. Next, attach a dummy load at J3 and apply

Fig. 4 — Close-up view of the r.f. attenuator assembly. The pilot lamps are mounted in $\frac{1}{8}$ -inch rubber grommets.

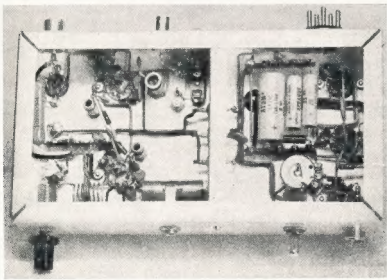
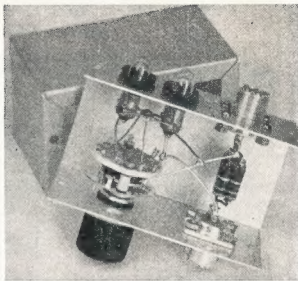


Fig. 3—Under-chassis view of the exciter, showing the r.f. circuitry in the left-hand compartment. The modulator is contained in the boxed-in area on the right.

power to the unit, using either crystal or v.f.o. control. The power swapper described later in this article will serve as a dummy load during tuneup and testing. A v.t.v.m., adjusted to read 0-15 volts d.c., can be attached between test point E and ground. Observing the reading on the v.t.v.m. meter, adjust L1 through L5 for maximum indication, which should be in the region of 5 volts after all stages are peaked. The spacing between L4 and L5 can be adjusted until optimum power output is secured.

The next step will be to neutralise the p.a. stage. Temporarily disconnect the plate and screen voltage from V2B and attach a sensitive r.f. sampling device at J3. The detector can be a 2-meter field-strength meter connected to the exciter by a short length of coaxial cable, with a 50 or 100-micro-ampere meter for an indicating device. Instruments of this type are described in the A.R.R.L. Handbook, under Measurements. Then the neutralising stub (black wire to the immediate right of L4 in Fig. 3) is moved back and forth near L4, with the exciter operating in the c.w. position, until a minimum reading is noted on the neutralising indicator's meter. The spacing shown between the stub and L4, in Fig. 3, is typical.

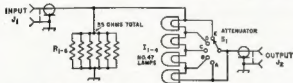


Fig. 5—Schematic diagram of the r.f. attenuator.

I1, I4, inc.—No. 47 pilot lamps.
J1, J2—Co-axial chassis connectors (SO-239).

In checking the modulator portion of the circuit, a No. 47 pilot lamp can be substituted for the dummy load at J3. Tune the transmitter for maximum bulb brilliancy by adjusting C2 and C3. With a crystal or ceramic microphone connected to J4, and with the switch S2 in the voice position, adjust R1 while speaking into the microphone. When the bulb shows an increase in brilliancy (about 25 per cent.), a suitable setting for R1 will have been reached. Further adjustment of the audio level can be carried out with the help of other stations after the transmitter is placed in actual on-the-air operation. If an oscilloscope is available, a more satisfactory setting for R1 can be established and will permit thorough evaluation of the exciter's waveform. This method is recommended if 100 per cent. modulation is desired.

THE SWAPPING DEVICE

Operating conditions for the transmitter are as follows: Oscillator plate current, 18 Ma.; tripler plate current, 10 Ma.; doubler plate current, 8 Ma.; final grid current, 1.5 Ma.; amplifier plate and screen current (combined value) 34 Ma.; modulator plate current, 50 Ma.

In some instances it will be desirable to include provision for attenuating the output signal from the exciter before applying it to a linear amplifier. It is better to "swamp out" a portion

of the excess r.f. drive than to detune the last stage of the exciter, or grid circuit of the linear, in an effort to reduce the level of signal input to the amplifier. The modulator portion of the exciter should at all times have a proper load to look into, which can only be maintained by permitting the p.a. stage to draw normal plate current. Do not reduce the coupling between L4 and L5 in an attempt to lower the output from the exciter unless the level of modulation is similarly altered.

If too much drive is available for your linear amplifier, the unit shown in Fig. 5 can be used. The swapper is housed in a 2½ x 2½ x 4-in. Minibox and has a step-attenuator switch which places as many as four No. 47 bulbs in series with the exciter's output. A 55-ohm dummy load, consisting of six 330-ohm 1-watt resistors, is permanently bridged across the input terminals of the swapper. This provides the exciter with a constant load and further attenuates the output signal. Depending upon the efficiency of the grid circuit in your linear amplifier, this accessory may or may not be required. The circuit for the swapper is given in Fig. 4. A more sophisticated version of this device, suitable for s.s.b. operation as well, can be

found in the 1965 edition of the A.R.R.L. Single Sideband Manual, page 238.

SOME FINAL THOUGHTS

The a.m./c.w. exciter can also be used as a low-power 2-meter transmitter for local operation, portable work, or during field-day activities. As an exciter, it will lend itself nicely to application with the 4CX250 2-meter linear amplifier described on page 11, February 1964, "QST." Other tubes, such as the 4X150A, operated Class AB1 can be driven to full rated input by this little exciter. By making appropriate modifications to the heater wiring, this unit will serve as a mobile transmitter. If you're interested in generating a clean a.m./c.w. signal for amplification by a linear amplifier—try this one. The usual circuit "bugs" have been eliminated.

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D.C. mA.—3, 30, 300.
D.C. Amps—3, 12. A.C. Amps—3, 12.
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SOME LOW-PASS FILTER DESIGNS FOR AMATEURS

J. McL. VALE,* VK5ZP

INTRODUCTION

In the last ten years or so the tremendous capacities of the modern digital computer have caused radical changes in the techniques of filter design and analysis.

The old image-parameter method of design, which Amateurs will have seen in the A.R.R.L. Handbook, is now quite out of date. No matter how closely the element values of an image-parameter designed filter agree with the design, the filter response, and in particular the attenuation outside the passband, will be significantly poorer than that hoped for in the design. In other words, filter design by the image-parameter method is imprecise and approximate.

Modern filter theory has discarded all the approximations of the image parameter method. It is now quite justifiable to attribute deviations between the response computed and that measured in practice to element value tolerances. Further, filters designed from modern filter theory will be more economical in the number of elements (capacitors, inductors) used.

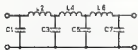
This article will give details of three low-pass filters. The author does not, at the moment, have the time for a more complete article, but if sufficient interest is shown he contemplates writing one in a few months time.

THE FILTERS

The basic circuit is shown in Fig. 1. The three filters described will have the following characteristics:

- (1) Maximum v.s.w.r. in passband = 1.10.
- (2) Cut-off frequencies:
Filter 1 35 Mc.
Filter 2 86 Mc.
Filter 3 150 Mc.
- (3) Input and output impedances—50 ohms.

FIG. 1 SEVEN ELEMENT LOW PASS FILTER

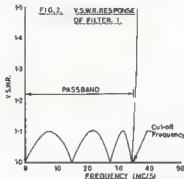


Computation of the element values requires specification of the parameters listed above. Conversely, changing either or both the cut-off frequency and the input-output impedance will require re-calculation of the element values. However, it will be shown later in the article that such calculations may be done easily with a slide rule or pencil and paper.

The reader will see what is meant by the first characteristic—maximum v.s.w.r. in passband—by examination of Fig. 2, which shows the v.s.w.r. of Filter 1. Note that the v.s.w.r. of the

filter is the v.s.w.r. measured at the input terminals of the filter when the output is terminated by 50 ohms (or whatever the specified output impedance is).

The cut-off frequency is defined to be that frequency at which the filter v.s.w.r. rises above the value specified as the maximum in the passband—see Fig. 2 again.



The attenuation of the three filters is shown in Fig. 3. Possibly the cut-off frequencies could be lowered somewhat, but it was thought that some allowance should be made for constructional errors. However, if you think you can get away with it, cut-off frequencies of 30, 54 and 148 Mc. would be ideal. As they stand though, the filters should be quite suitable, especially the h.f. filter (Filter 1) and the six metre filter (Filter 2).

The response of the two metre filter (Filter 3) is not very satisfying, although it is optimum for a seven-element filter. Adding two or four

more elements would improve its response, but the element values would then be quite different and the author just does not have the time to calculate them at present.

The attenuation graphs are a little misleading in one respect—the attenuation does not fall to zero in the passband; in fact the attenuation in the passband (neglecting coil losses) is so small that it cannot be shown on the graph.

ELEMENT VALUES

Element	1	2	3	Units
C1	72.5	45.3	16.9	pF.
C2	159	99.4	37.1	pF.
C3	159	99.4	37.1	pF.
C4	72.5	45.3	16.9	pF.
L1	317	198	73.9	nH.
L2	371	232	86.6	nH.
L3	317	198	73.9	nH.
	1 pF. = 10 ⁻¹²			Farad
	1 nH. = 10 ⁻⁹			Henry

Tolerances: Plus or minus 1% tolerance on element values will not degrade response markedly. Capacitors then should be no problem.

The inductors are best made by bringing them to resonance with the filter capacitors. That is,

For Filter 1—

C1 and L1 resonate at 33.2 Mc.
C2 and L2 " " 20.6 Mc.
C4 and L3 " " 33.2 Mc.

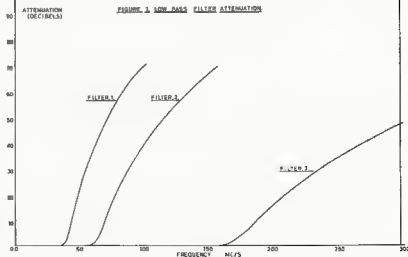
For Filter 2—

C1 and L1 resonate at 53.1 Mc.
C2 and L2 " " 33.2 Mc.
C4 and L3 " " 53.1 Mc.

For Filter 3—

C1 and L1 resonate at 144.2 Mc.
C2 and L2 " " 89.3 Mc.
C4 and L3 " " 144.2 Mc.

(Continued on Page 12)



* 29 Canton Road, Gawler East, South Aus.

SWAN SW350 MARK III.

My competitor seems to be quite upset by the effect of something he started himself when he introduced the Swan 350 Mark II. In July, 1965. This was when Swan Co. of California added full 10 M. coverage, VFO trimmer and VFO ceramic coils to their transceivers, but Swan Co. never made a distinction between their earliest and latest models SW350—they are all plain SW350 to them.

However, these first modifications to the SW350 did not fully cure the drift in the VFO and Swan Company admitted that in a Service Bulletin dated 1st October, 1935. Incidentally, you will not get a copy of that Bulletin, regardless of whether your set is registered in California, where it should be registered, or in Sydney. Swan Company stated that the VFO drift was their major problem with the SW350, regardless of the ceramic VFO coil forms, and then decided, in October, 1965, to cut a hole in the transceiver bottom cover, mounted the VFO transistor on a separate panel against the bottom plate as heat sink and, at the same time, incorporated for the first time in their 4 years' history, a crystal filter unit made elsewhere. This new filter has a narrower and different filter passband response, a feature that others apparently overlooked entirely. I considered these modifications just as important as the reasons for the Mark II classification and christened this latest Swan SW350 the Mark III. However, I did not start this ball rolling and it is too bad that one's own medicine now tasted bitter.

Anyway, this "retailer," who imported over 150 transceivers in 2 years' operation, will continue to be on the alert for significant new developments in Swans and other overseas brands, and will announce the Mark IV, whenever justified. This is in compliance with my self-assigned task to bring the Australian Amateurs the best available at the lowest cost. Without my activities the public would most likely still be paying at the 1963/64 rate of £270 for a U.S. \$275 single-band transceiver and £285 for a U.S. \$320 tri-band transceiver instead of much more value now in a U.S. \$395 five-band transceiver for even less money. Import duties and sales tax burden the cost of imported equipment already more than many purses can afford and the local tariff-protected manufacturers apparently cannot compete. I personally brought the first Swan SW350 transceiver, ever imported in Australia, to two Sydney firms with a blank order to make me 50 similar sets, but they never made me a quote.

As added features from now on my Swan SW350 Mark III. will include USB/LSB sideband selection and a 100 Kcs. crystal calibrator at no extra cost. Also the Galaxy V. will have the crystal calibrator as standard equipment, making both five-band S.S.B. transceivers real bargains at A.\$900, which also includes a heavy duty 240v. a.c. supply/speaker unit in matching cabinet.

Yes, sideband selection and crystal calibrators as standard equipment at no extra cost!

This "retailer," exclusive importer of Galaxy, Drake, Aztec, Hy-gain and Autronic, appointed distributor by the world-wide export agent for Swan Co., with more new and interesting lines to be introduced in future (German origin) continues to offer fully imported gear at the lowest prices, with full after-sales service and warranty. Unsolicited comments by:

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- (b) "With my large full size 40 metre rotary beam I pick up strong local signals outside the Amateur bands that produce spurious responses in other transceivers, but not in the Galaxy III. when properly aligned."

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Swan SW350 Mark III. or Galaxy V.: USB/LSB sideband-selection, 100 Kcs. crystal calibrator and 240v. a.c. supply speaker unit included, A.\$900.

AZTEC 12v. d.c. supplies, A.\$90 and A.\$110.

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10/15/20/40 meters vertical, 14AVQ, A.\$44. 10/15/20/40/80 meters vertical, type 18AVQ, A.\$70. 10/15/20 M. 3-element junior beam, TH3JR, A.\$96, same as senior model "Thunderbird" TK3 MK. 2, A.\$140. 6-element 10/15/20 M. beam, type TH6DX, A.\$200. Hy-gain mobile mounts in various types.

Antenna-rotators: Alliance U-98, A.\$55; CDR TR-44, A.\$90; CDR Ham-M, A.\$180. All for 230 v. a.c. with indicator/control units.

USED EQUIPMENT, RECONDITIONED A-1

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Hallcrafters HT-37 all band S.S.B. Transmitter, A.\$275.

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SIDEBAND

Sub Editor PHIL WILLIAMS, VK6NN

S.S.B. CONVENTION

The second Sidebanders' Convention was held at Hamilton, Victoria, during the long week-end at the end of January, when about 60 users of the s.s.b. mode of transmission gathered. These meetings will be held probably every two years, as those present consider this gives them the opportunity to get along every time. The first was held in May, 1964. The main organiser for the recent function was Ern VK3AEM, assisted by Dan 3ADD, Tim 3TW and last but not least, Ian, an enthusiastic listener.

The main feature of this Convention was its informality to give people a chance to get to know better those whom they have contacted over the air. The Buffet Dinner on Saturday evening and the following Sunday morning lectures were enjoyed by all. Delegates with mobiles were "talked" into Hamilton via the station lent by Fred 3YS.

Lectures were delivered by Geoff VK3AC on "Mobile Antennae," Aris VK2AYA on "Recent Trends in Sideband Equipment" and Phil VK5NY on "The Complete Sidebander," after which delegates departed for home, although a few remained at the motel for an extra night to enjoy additional Hamilton hospitality and travel home on the Monday holiday.

Those who missed going to Hamilton '68 should make a note to book in early for Hamilton '68, which is sure to be bigger and better.

LINEAR AMPLIFIERS

Following many requests, the next few months of sideband notes will be devoted to the subject of amplification of the final frequency single-sideband signal, from the low level output of the last mixer in the transmitter, to the full power of some hundreds of watts "peak envelope power" (p.e.p.). I shall not state here what the actual power level permitted by the P.M.G.'s Department is, as this is not yet defined and is the subject of current negotiations with the Department. What ever this level will be, the principles will be the

same, the power, current and voltage levels will be within 2 or 3 db. or less than half an "S" point.

We will be mainly concerned with optimum operation of the various stages, from say the class A pentode or tetrode with an input signal of less than 2 volts across a high impedance tuned circuit, to the class B linear power amplifier. The ease and convenience of tuning, band changing, broad banding, maintenance of stability, reduction of intermodulation distortion, proper loading and reduction of radiation of unwanted signals are all very important, and it is hoped to provide some useful tips for the home designer and constructor.

in a box on its own for this reason alone.

Fig. 1 shows a typical block diagram of the recommended arrangement. It is only fair to mention that the class AB1 stage in the exciter may be lifted to the "hundreds of watts" level by adding more tubes of the t.v. line time-base type, e.g. 6DQ5, in parallel and increasing the plate voltage to the 1000v. region, however, this is not recommended as problems such as current sharing, neutralisation, high grid circuit capacitance, and, most important, the heating of v.f.o. components in the vicinity, to say nothing of the increased intermodulation distortion, may become apparent.

It is far better to drop back the level of output required from the exciter to reduce distortion and heating, and use this to drive a conservatively designed (and operated) linear amplifier, rather than to attempt to push the exciter too hard.

As a general rule it is necessary to operate the final linear amplifier with high plate voltage and lower the current requirements for the same power output. As an example it is quite safe

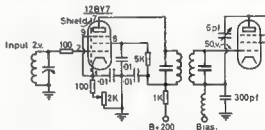


Fig.2 Typical class "A" driver stage - Gain = 25. (approx)

It is usual to employ a 3-stage amplifier at the final frequency to provide the gain mentioned above with all of the desirable features. The first two stages are included within the s.s.b. exciter, the first being class A, and the second a class AB1 amplifier. The final linear stage may be completely separate, and it is desirable to keep it separate, complete with its own power supply and mains r.f. filtering, as the high voltages and currents in the plate circuit can cause havoc with low-powered audio stages, oscillators and mixers in an exciter. It has been known for power increases from the 50 to 100 watt level to the 500 watt level in the shack to cause all manner of troubles. It is a very good idea to keep the final linear

to operate 807's as linear amplifiers with 1000 to 1200 volts on their plates, i.e. twice the steady plate voltage applied to a plate modulated stage.

Valves known to have good linearity, and most transmitting valves come in this class, may be operated conservatively in neutralised, conventional amplifier circuits using tuned plate and grid circuits with appropriate supply voltages. Passive grid circuits, i.e. a low value grid resistor of 50 to 200 ohms, may be used if sufficient drive is available, and neutralisation omitted—this applies to tetrode or pentode stages. Where linearity is not a feature of the tubes to be used, such as the t.v. line-time-base tubes, then neutralisation

(Continued on Page 12)

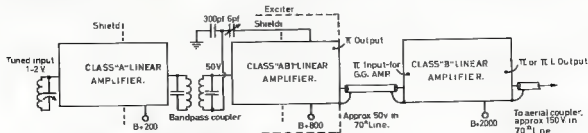


Fig.1. Typical final frequency amplifier for SSB transmitter.

SIDE BAND

(Continued from Page 11)

tion and negative feedback are desirable if they are to be operated at high level.

The application of negative feedback to r.f. linear amplifiers is not for Amateur designers, except—and there is only one exception—in the case of the grounded grid amplifier, but there are some tricks and precautions to be observed, and these will be outlined later.

THE CLASS "A" AMPLIFIER

There is not a great deal of choice of suitable valves for this stage, but some tricks of the trade—not always realised by the trade—are worth consideration. Suitable tubes are the 6AG7, 12BY7, 6CL6, 6CH6 and 6BT6, but the various audio output tubes, e.g. 6V6, 6BM5, 6L6, 6AQ5, are less suitable due to their high plate to grid capacitance, which makes stable operation difficult. Twin triodes have been used as cascode amplifiers, and I have used an EI80CC computer triode with a Gm of 6800 quite successfully.

Coming back to the first series of video-type tubes, examination of operating conditions shows that most manufacturers invariably put too many volts on the plate and screen and then have a heat problem. Since 50 volts of peak output is required to drive the next stage, then 150 to 200 volts on the plate and screen is more than adequate. The plate current may be run at 30 to 40 milliamperes for less than 8 watts of plate dissipation, which allows the stage to

operate into a lower plate load, with better linearity, and much higher sensitivity. The advantages are obvious, and the result enables us to use a supply of about 180 volts for the whole of the low level section of the exciter, including the screen of the class AB1 output stage. The reduction in heating in the exciter is important and results in less v.f.o. drift.

Fig. 2 shows a typical 12BY7 driver stage, a tube type currently used as a video stage in Australian t.v. receivers and readily available at a reasonable price. This is a high slope tube and needs to be given all of the shielding and grid-stopper treatment for stable operation. With this it is a good performer.

[To be continued.]

LOW PASS FILTER DESIGNS

(Continued from Page 9)

FILTERS FOR OTHER FREQUENCIES

If one has the element values for a filter of cut-off frequency f_c and one wants to design a filter cutting off at f_s , simply multiply all element values by the ratio $(f_c \div f_s)$.

FILTERS FOR OTHER INPUT/OUTPUT IMPEDANCES

The filter values listed above are for input and output impedances of 50 ohms. Conversion to other values—say 75 ohms—is a matter of multiplying all inductances by $(75/50)$ and all capacitances by $(50/75)$.

USEFUL REFERENCES

- (1) "Network Analysis and Synthesis," L. Weinberg, McGraw Hill, 1962, p. 601-670.
- (2) "Reference Data for Radio Engineers," International Telephone and Telegraph Corporation, 4th edition, 1963, p. 37-225.

W.I.A. D.X.C.C.

Listed below are the highest twelve members in each section. New members and those whose totals have been amended will also be shown.

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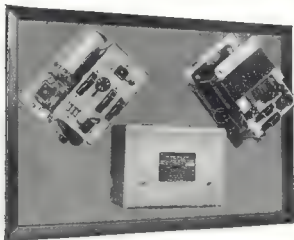
Call No.	Cr. Cont. No. rise	Call No. rise	Cr. Cont. No. rise
VK6MS	34	VK2JF	81
VK1AHO	31	VK4HR	12
VK6RU	2	VK2ADE	65
VK6AB	45	VK2TL	28
VK6MK	43	VK1AAK	38
VK4F7	31	VK6KW	4
New Members:			
VK6CM	69	VK3SM	70

C.W.

Call No.	Cr. Cont. No. rise	Call No. rise	Cr. Cont. No. rise
VK6KE	10	VK1AGH	71
VK3CK	38	VK1ARQ	79
VK3GL	5	VK2EO	2
VK4P7	28	VK6RU	15
VK1ADE	31	VK3ARX	65
VK3NC	19	VK3XB	75
Amendments:			
VK4HR	8	VK2RK	33
VK3TL	78		

OPEN

Call No.	Cr. Cont. No. rise	Call No. rise	Cr. Cont. No. rise
VK1ADE	38	VK3NC	71
VK6RU	5	VK4HR	7
VK1AGH	63	VK3VN	18
VK6MK	74	VK3JA	43
VK4P7	33	VK3TL	85
VK3ACK	6	VK1AFK	32
Amendment:			
VK3TL	58		



Illustrated. Top left—Unregulated Power Supply—output 48V. 750mA. Right—Frequency Changer output 75V., 20VA., 25c/s.

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L.M. 52

MODIFYING PALEC VALVE AND CIRCUIT TESTER

(Continued from Page 2)

voltage to suit, then move slide switches to select valve pins, and insert valve in socket.

"Element Shorts". Set function switch (bottom l.h.s.) to "Element Shorts" and move each slide switch in turn to the "Test" position and return to "Common" position, with the exception of the two selected filament switches. Any continuous glow of the neon globe will indicate which element of the valve has an element short, or is internally connected.

When a valve is found with a short, don't test, but tip it out in the w.p.b.

Emission Test: Set function switch to "Merit Test" position. Set "Range Control" to "Palc" test chart number for the valve under test. Depress "Press for Merit" button and read the meter for valve condition, after having ascertained and selected the slide switch for the grid or diode connection under test.

After having completed valve testing, return all slide switches to the common position, as you may leave the filament selector switch on 12v. and come back to test a 1.4v. valve with rather disastrous result to the valve.

Make it a habit to set all selector switches to the correct positions before inserting the valve in the socket.

VK-ZL CONTEST RESULTS

(Continued from Page 13)

Europe

DJ6QT	3312 pts	OH7TV	80 pts
DJ7LD	304 "	OR8NC	Check
DM2ATD	64 "	OK1ADP	729 pts
DL1SV	90 "	OK1ARV	72 "
DL7AA	2128 "	OZ3SK	570 "
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LIGHTNING

• The effects of lightning on electric reticulation systems are of great importance to all electric supply authorities. The Sydney County Council maintains a standing committee which keeps the lightning performance of its system under constant review. This committee also ensures that the Council incorporates the latest and most suitable lightning practices.

of the manner in which the electric field changes produced at the ground by lightning flashes varied with the distance from the storm. He concluded that, in a thundercloud, the upper part is positively charged and the lower part is negatively charged. This deduction has been confirmed by later work.

As the storm progresses it develops an increasing electric potential between its separate parts, neighbouring clouds or the earth. This potential is developed by the gradual accumulation of charge believed to be built up by the action of falling rain, snow, ice pellets, or some other unknown natural process.

Potential differences may reach values as high as 100,000,000 volts. The transient currents produced are in the range of from 3,000 to 200,000 amperes.



Fig. 2



LIGHTNING—THE ELECTRICAL DISCHARGE

It is believed that lightning strokes may be started with potentials of the order of 5,000,000 (or more) volts between cloud and earth.

Photographs of lightning strokes have been taken by a special moving camera based on a design by Sir Charles Boys. Use of this camera has disclosed that the lightning flash consists of a number of successive strokes which follow the same track. These strokes occur at intervals of 1/100th of a second, and the average number of strokes is three.

However, as many as 47 have been recorded in a single flash.

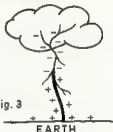
A lightning stroke is initiated by a streamer or pilot leader developing downwards to the earth from the negatively charged base of the cloud (Fig. 1). The current in the leader is not high, probably less than 100 amperes.

As the leader approaches the earth the gradient at the earth's surface becomes great enough to cause a short streamer to rise from the earth (Fig. 2).

Eventually contact is made and the high current flow associated with lightning occurs (Fig. 3).

This high current flow has a short duration peak and is followed by a low current long duration tail (Fig. 4). The low current long duration portion of a stroke is not disruptive, but will cause fires in flammable material. For that reason, low current lightning is known as "hot" lightning.

It is the so-called "cold" lightning, with its high current peak, that is so damaging to electrical apparatus and reticulation systems. Its destructive effects are seen in any high resistance medium. A lightning discharge flowing in a good conductor earth will not injure that conductor.



Most lightning discharges occur within the cloud itself. The higher the cloud the easier it is for the discharge to pass between the upper (positive) and the lower (negative) sections of the cloud than it would be for a cloud to ground stroke.

Internal flashes do not usually appear as lightning strokes, but rather as general illumination in the cloud. This is due to the refraction of the light on the myriads of water droplets within the cloud.

There is no known method of either preventing or resisting the power of lightning strokes. For the time being, mankind has to put up with them. All the electrical engineer can do is to co-exist with lightning and to divert it from installations where it can do damage.

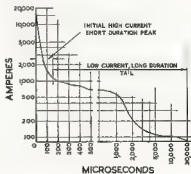


Fig. 4. Record of current in a direct stroke to the Cathedral of Learning, University of Pittsburgh, June 10, 1939.

THE maxim, beauty lies in the eyes of the beholder, is particularly apt when applied to lightning. Views range from beautiful, but awesome, to terrifying, dangerous and destructive.

It is the dangerous and destructive properties of lightning that concern the electrical engineer. The high voltages in a lightning stroke create problems that he must overcome if interruptions to supply are to be avoided.

Every day there are approximately forty-four thousand electrical storms throughout the world. It is estimated that the actual number of lightning strokes total about one hundred per second.

There is little chance of being killed by lightning unless one is foolhardy. During a thunderstorm it is hazardous to play golf, swim in open water, stand under an isolated tree, fly a kite, or generally remain in the open. Prudent people shelter during storms. The safest shelter is a metal enclosure such as a car or metal-framed building.

Despite almost two hundred years of scientific enquiry, the exact processes which give rise to a lightning flash are unknown. Many organisations are either conducting research or seeking the answers to the problems associated with lightning strokes to electrical apparatus.

The brevity of the average lightning flash, about 1/100,000th second, hampers studies in the field. Most research must be conducted in the laboratory by examining the behaviour of artificially created storms.

Benjamin Franklin was the first to identify lightning as an electrical discharge. During a thunderstorm in 1752, he was able to produce sparks from a key attached to the end of a kite string. Since then various theories, none of which meet with universal acceptance, have been advanced to account for the origin and generation of lightning.



Fig. 1



THUNDERCLOUDS—ELECTRICAL BUILD-UP AND STRUCTURE

A thunderstorm appears to be a form of electrostatic generator producing both positive and negative charges. The charged particles then become separated into groups of positive and negative charges in different parts of the cloud.

C. T. R. Wilson was the first man to deduce the charge distribution within a thundercloud. He did this by a study

Reprinted from "The Constructor," September, 1964.



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LIGHTNING PROTECTION

Protection from lightning is achieved by either one of two methods or by a combination of both.

Shielding is the provision of a conductor which intercepts the lightning stroke and conducts the electrical discharge harmlessly (it is hoped) to earth.

The other method is by the use of lightning arresters. By providing a by-pass around insulation, these allow current in a reticulation system to leave without causing either damage or an interruption to supply.

SHIELDING—USE OF LIGHTNING CONDUCTORS

Lightning conductors, which take many forms, shield a building, free, mast or other object by attracting flashes which would otherwise strike either the object on which the conductor is placed or its immediate surroundings. Having attracted the stroke, the electrical discharge is passed to the earth.

When the path of a pilot leader approaches the earth remote from a conductor its course will not be influenced by that conductor. An upward streamer starts from the earth itself and the stroke is completed (Fig. 5).



Fig 5

Should the pilot leader be close to the conductor the potential gradient experienced at the end of the conductor produces a short upward streamer from the conductor. This upward streamer meets the pilot leader and the contact is made. The subsequent lightning discharge flows to earth via the conductor (Figs. 6 and 7).

Any lightning stroke headed towards the earth within a certain distance of a conductor will be attracted to that conductor. The area of attraction surrounding a conductor is known as the shielded area.

Good shielding is provided when out of every 1,000 lightning strokes only one strikes the shielded object, the other 999 being attracted by the conductor. This is known as an exposure of 0.1 per cent. The shielded area depends upon the configuration of the conductor. In the special case of a rod or mast the shielded area is that covered by a cone whose apex is the top of the conductor with its surface forming an angle of 30 degrees to the vertical (Fig. 8).

The only way to ensure complete protection from all strokes is by practically surrounding an object with a conducting shield.

Multiple rods increase the shielded area between them to a greater extent than the sum of their protected areas.

This increase, although appreciable, may not be generally recognised.

A popular fancy is that lightning current has a tendency to jump from any sharp bend in the conductor. This type of flash-over occurs only when a nearby object offers an easier path to earth than does the conductor itself.



Fig 6

The prime requisite with all shielding devices is that they be well earthed. Failure to ensure first-class earthing can mean damaging side flashes as the discharge seeks an easier path to earth.

Possibly the earliest use of lightning rods or conductors to provide effective shielding was in the 19th century. Lightning conductors were fitted to the masts of the wooden ships used by the Royal Navy.

High voltage transmission lines are usually shielded by means of one or more wires suspended above the line conductors. These wires are earthed through each tower. When erecting transmission lines, engineers make a thorough check of the earthing of each tower. If found to be inadequate, long wires known as counterpoises are bonded to the tower and buried in the ground to form a radial pattern around it.

Shielding will not prevent the line conductors from being subjected to transient voltages during a lightning stroke. However, it will usually keep the transient voltage below the flash over voltage of the insulators.

LIGHTNING ARRESTERS

Protection of equipment is usually carried out by means of surge diverters, more commonly known as lightning arresters. These devices provide an easy path to earth for the lightning current, yet prevent the normal supply current from following. Once the lightning current has been passed to earth the arrester must rapidly re-establish itself as an insulator to prevent power current following.

The name "lightning arrester" is not really correct. The device is actually a lightning diverter and a power current arrester.



Fig 7

(Spark gaps are sometimes used instead of arresters. They are less expensive and if the gap spacing is correctly chosen they will prevent damage to costly apparatus, but do not avoid interruptions to supply.)

Lightning arresters are generally of two basic types: expulsion arresters and valve arresters.

The expulsion arrester consists of a tube with an electrode at each end. The tube is made of a material that, under the heat of an arc, will create a gas (the tube may even be filled with gas-producing material).

In operation, the lightning current causes the electrode gap to break down. An arc is formed and this is maintained by the power supply voltage. The heating liberates gas at a rapid rate and the arc is blown out of the tube by the gas, lengthening it and interrupting the power follow-on current.

As the explosive nature of the discharge is related to the fault current there is a maximum current which an expulsion arrester can handle. Such arresters are usually employed on systems with moderate fault duty.

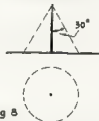


Fig 8

The rapid arc extinction of the expulsion arrester can give rise to transient overvoltages which are damaging to certain types of equipment.

The so-called valve arrester avoids this trouble and is consequently more often used.

It consists of a number of arc gaps in series with blocks of resistance material having an inverse resistance characteristic, i.e. the resistance decreases as the voltage increases.

At high lightning voltages the blocks have negligible resistance to the passage of current. At the lower power frequency voltage their resistance has increased and the current is reduced to the point where it can be interrupted by the gap.

The process described is a more gradual way of preventing follow-on power current than that employed by expulsion arresters. Both types of arresters divert the lightning current to earth yet avoid power interruptions.

★

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concerning miniaturisation of receivers and transmitters, finally coming out with the statement that he had been experimenting with a small transistor for W.L.C.W. and he was hurriedly rushed to the tent of the emergency and set up in a jiffy. His troubles apparently had been many and varied, although his last prototype had been small enough to be carried by a large camel or possibly a three-quarter size elephant, although he felt that he would be able to get it even a little smaller with a squeeze. He was cut to the quick with my suggestion that his appearance at the scene of any emergency, accompanied either by a camel or an elephant, would be enough to and any emergency, but when I said, as I was leaving the meeting, "Good-night Elephant Boy he gave me an excellent imitation of the caretaker's Alsatian, so much so, that I waited not upon my orders to depart."

Our revered and respected President, Ross KP, can sit back on his laurels now that the first year of his reign has ended, especially as he now holds the record of having been chairman of the shortest annual general meeting in the history of the Division. I wonder just what his secret is.

A witty bird is our Arthur GHV, at the meeting before the last he came and sat near Albert ELL and myself, and proceeded as usual to give me my usual earbashing on the merits and demerits of "The Thing". Although my ear was trailing on the ground when he finished, I was able to resist his attack, settled myself on the bench as to my solidarity. How simple can I be? He came up to me at the meeting this month and nonchalantly remarked, "see that Albert ELL has become a member of the s.a.b. fraternity." "He was so interested in our conversation at the last meeting that he bought a commercial job and is tickled with the results." That settles it. I am going to sit in a corner all by myself at future meetings, nobody is going to use me as a stooge for "The Thing". I must be getting old. I will be failing to the thimble and pea set before long!

Well, this has been such a dismal month, one way and another, that I am going to stop now—why is everybody cheering?—even though

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the notes may be a little shorter than usual, then, but don't despair, this is only a temporary feeling of frustration, and I will be back next month, better than ever. The Publications Committee and the Editor being willing. What's that?—Why worry to come back?—Throw that VKA out!

73 de 3PS—PanSy to you.

TASMANIA

By now our Annual General Meeting and Dinner is over, and your new Council has been elected. On their behalf I thank you for the confidence you have shown, and as in the past I know the business of the Institute is in good hands.

We must of course say farewell to our three Councillors who did not seek re-election this year, they are: Ted TBS and Charlie TK5—all key men in Council for the last couple of years at least. Thanks to each of you from all of us for a job well done. Let's hope we'll see you back one day.

Keith TRX has gone sideboard with a home-brewed along with the phlegm and the show around at the March meeting and it appears to be a f.b. rig, built in true TRX construction. Tom TAI, is in the process of building a 40 W. rig, and I am sure that it won't be long before we hear "Uncle Tom" on the bands again (not before time either).

Ian TZZ is in the process of acquiring himself a 48 ft. tower, which he tells me he's going to top with a 3-band quad—as if he doesn't work enough DX now—he'll never go to bed at all when the bands are open.

Our loss is someone else's gain, and this is very true in the case of Doug TIZ who is leaving the Division to take up an important city of Canberra. Good luck Doug, hope to hear you on the bands in the not too distant future. We'll always be interested to hear from you.

With official approval for slow Morse transmissions to hand we have three sessions each week on the 3.5 and 7 MHz bands for the island. The time is 8 p.m. on Sunday, Tuesday and Thursday evenings. Don't forget chaps, you still have to be at the service, let the operators know, we had trouble once before, the operators spent hours at his rig, and to my knowledge never returned, but even now, whether anybody took advantage of the service—most disheartening I think you will agree.

Earlier this upon us again, which of course means Convention time, all conventions are important, but this year's should be more important than any other, as the matter of service should be, we hope, finalised. Then it's up to the Attorney-General. We wish the conference this year as an other year, very busy. Incidentally we may lose our Federal Councillor, Ted YBJ, in the latter part of the year. He tells me there's a chance he may go to Darwin, but he has been told to keep in the past where he can go, but no one ever thought he'd take us seriously—for VKT's sake we all hope you can delay it for another year if not longer. Ted, but as someone once said, "When you gotta go ya gotta go," and that's about what I'll do.

Hope everyone who attended the annual meeting and dinner enjoyed themselves, and we'll see a few more still at next year's function. 73, Geoff TZAX.

HAMADS

Minimum 5/-, for thirty words.
Extra words, 2d. each.

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FOR SALE: R1155B Receiver in excellent condition, complete with power supply and speaker, \$49. VK2TS, R.M.B. 100a Mangrove Mountain, N.S.W.

FOR SALE: 3 in. CRO type MD/32 separate P/S and handbook, \$25. Brand new and unused Collaro mono tape deck, \$40. 6 meter Converter with all valves (E88, 2 off BL8) and xtal for 4 Mcs. i.f., \$10. Power Supply—1000v. 300 mA. (trans. tapped at 850/750/550) and 400 v. 250 mA., all on one chassis, \$25. AMR101 Comm. Receiver. Made by A.W.A. and modelled on National H.R.O. Coil boxes 900 Kcs. to 30 Mcs. Separate power supply operates on either 240v. a.c. or 12v. d.c., \$70. 2 metre Tx. Runs 15 watts to 3/12. Complete with modulator, power supply and microphone on two 3 1/2-inch sections of standard rack panel, \$30. Vox unit—complete with all tubes and 10K relay on 3 1/2-inch panel, \$15. Prices open to negotiation with H. L. Hepburn, VK3AFO, 4 Elizabeth St., E. Brighton, Vic. Tel. 96-2414 evenings and weekends.

HANDBOOKS available for ATR2A, ATR2B, ATR4A, ATR13B/AT13C, AT14A, AR17, AMT150. Best offer. VK3AXK, 28-4968.

SELL: Geloso G2227R Transmitter, as new, £60 (\$120). Has had very little use. M. Saunders, VK3AMV, 106 Victoria St., Warragul. Phone 21218.

SELL: Hallicrafter S36B Communications Receiver, 5 tube, 4 band, converted power supply for 240v. operation. Excellent condition and performance. \$40. J. D. Fargie, 26 Veronica St., Lower Ferntree Gully, Vic.

SELL: 5 ft. cabinet-type rack with 144 Mc. xtal contr. x-mtr. QQE08/40, 80 w. inp.; v.f.o. contr. 52 Mc. x-mtr. QQE06/40, 80 w. inp.; Modulator 2 x 807 in AB1; Plate and screen mod.; Sidetone osc.; DGT-5 C.R. tube; Power supply 600v. 400 mA., 300v. 150 mA., 24v.; Meters: 0-10 mA. grid current, 0-250 mA. plate current, 0-1000v. plate voltage; everything is relay controlled, \$195 or near offer. C. Haggart, VK5CSW, Lot 25, Larkdale Av., Paradise, S.A.

WANTED for Youth Radio Club; BC221 Frequency Meter or similar, with calibration book. Price and details to VK2AXC, 78 Aberdare Road, Cessnock, N.S.W.

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$$v = c \left[1 - \left(\frac{1}{eVa / (300 m_e c^2) + 1} \right)^2 \right]^{\frac{1}{2}}$$

?

Most people go happily through life without ever needing to solve an equation from the time they leave school. But in the vastly complicated world of electronics, such equations are indispensable for reducing complex problems to simple terms. An example is the equation illustrated above. This equation provides the velocity which an electron will attain in its travel through a picture tube electron gun. It is interesting to note that, with a nominal anode voltage of 16,000 volts, the velocity of the electron will be approximately 170,000,000 miles per hour which is one quarter of the speed of light.

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